

Stormwater Concept Plan

Bonterra Subdivision

Chatham County, NC

Prepared by:



PENNONI ASSOCIATES INC.
CONSULTING ENGINEERS

February 16, 2018



Project Description

The existing site consists of two (2) parcels (AKPAR 2532 & 2533) totaling 31.495 ac +/- . There are two (2) residential dwellings and associated structures and improvements presently on the site; all existing improvements shall be removed with this project. The proposed development will consist of a maximum of twenty-two (22) single-family residential lots with a minimum lot size of 40,000 sf. To access these lots, a proposed roadway will be constructed off Mann's Chapel Road. The proposed roadway will be paved (18' wide with shoulder section) and constructed to NCDOT standards. There is a natural stream crossing the site from west to east. In order to construct the proposed roadway, a stream crossing will be required. At the easterly end of the on-site stream there is an existing small pocket of wetlands; this area will not be disturbed. Stormwater will be designed in accordance with the Chatham County Stormwater Ordinance and NCDWQ standards.

Existing site conditions

The existing site is located near the top of a drainage shed. There is a stream running from west to east across the site, with a small pocket of wetlands near the eastern property line. The stream begins just below a farm pond to the west of the site that has a drainage area of approximately 20.22 acres. This pond is not engineered and does not have a control structure or weir. Approximately 60% of the site drains to the stream, as well as approximately 7.65 acres from the north of Mann's Chapel Road that enter the site through 15" RCP and 18" RCP pipe culverts running under the road. The southern portion of the site drains to a swale near the southeast corner, with a small percentage of the site draining to the eastern boundary by sheet flow. See SWM-1 for the existing drainage plan. Computations are located in Appendix A.

The site is primarily wooded, with small cleared areas around the existing buildings and improvements. The northern portion of the site from Mann's Chapel Road to the stream consists of Helena (HeB) and Vance (VaB) soils, which are both hydrologic group C. The site to the south of the stream consists of Wedowee (WdC, WdE and WeB) soils which are hydrologic group B.

Proposed Water Quality Devices

This proposed site is a relatively low-density development, with the total impervious area limited to approximately 9,000 sf per lot, plus 0.76 acres of impervious pavement of the road. The site is generally divided into two drainage areas, with the high point of the road being the main divide. It is the intention of this design that the majority of impervious site area will be captured by a water quality device, and the untreated area will be undisturbed forest or graded pervious area which will maintain existing drainage patterns. See SWM-2 for proposed drainage divides and water quality treatment locations.

The water quality treatment to the north of the high point will consist of treatment swales along the ditch section of the road. Check dams will be provided at a maximum spacing of 200 feet along the road. This maximum spacing allows the velocity within the channel to remain below erosive velocities and the swale will drain within 72 hours of a rain event. The swales will treat the water draining from the road and from at least the front 40 feet of the lots. Additional area captured by the swale will depend on the natural topography of the area. The lots to the west of the proposed road generally drain toward the road, and lots to the east generally drain to the rear of the lot and to the stream. The final location of the check dams will be determined based on final site plan design. See Appendix B for typical drainage swale computations.

The water quality treatment for the southern drainage area will consist of a bioretention basin that will treat 0.27 acres of road plus the impervious area of five (5) lots. The basin will be located within a 50' stormwater management easement along the southern property line. The runoff from the road will be collected in an inlet at the end of the cul-de-sac and directed to the bioretention cell either by pipe flow or a swale along the western property line of lot 12. Offsite area to the west of lot 12 will be directed around the basin. The basin was sized per NCDWQ standards to treat an area of 4.60 acres, of which approximately 30% is impervious area. See Appendix C for bioretention basin computations.

Downstream impacts from the proposed development will be analyzed using the Ten Percent Rule. This is shown on SWM-3 attached to the back of the report.

Stream Crossing

The proposed road design will require a stream crossing. This crossing will consist of a box culvert installed in accordance with NCDOT standards. The box culvert is sized to pass the 1-, 2-, 5-, 10- and 25-year, 24-hour design storm events, as well as provide at least two (2) feet of freeboard to the shoulder of the road for the 100-year, 24-hour storm event. The drainage area to the culvert includes the 20.22 acres to the pond at the top of the stream. Since the pond is not an engineered pond, the T_c was computed as if any water that enters the pond leaves immediately. It was determined that a 4'x3' box culvert is adequate for this stream crossing. See Appendix D for culvert design computations.

Appendix A

Existing Conditions Drainage Computations

Worksheet 2: Runoff curve number and runoff

Project	Mann's Chapel Road Subdivision	By	MAG	Date	2/8/2018
Location	Outfall #1	Checked	BTN	Date	2/8/2018

Check One: Pre-Developed Developed **Pre-Developed Conditions - Outfall #1**

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN*			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi ² <input type="checkbox"/> %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
C	Residential (1 acre average lots)	79			34.97	2762.6
B	Residential (1 acre average lots)	68			15.73	1069.6

* Use only one CN source per line

Totals				50.70	3832.27
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CN (weighted) = $\frac{\text{total product} = 3832.27}{\text{total area} = 50.70}$

Use CN **75.59**

2. Runoff

	Storm #1	Storm #2	Storm #3
Frequency..... yr	2	10	100
Rainfall, P (24-hour)..... in	3.57	6.13	7.67
Runoff, Q..... in	1.39	3.45	4.81

(Use P and CN with table 2-1, figure 2-1, or equation 2-3 and 2-4)

Worksheet 3: Time of Concentration (T_c) or Travel Time (T_t)

Project	Mann's Chapel Road Subdivision	By	MAG	Date	2/8/2018
Location	Outfall #1	Checked	BTN	Date	2/8/2018

Check One: Pre-Developed Developed **Pre-Developed Conditions**

Check One: T_c T_t through subarea

Notes: Space for as many as two segments per flow type can be used for each worksheet.
 Include a map, schematic, or description of flow segments

Sheet Flow (Applicable to T_c only)

Segment ID	A-B		
1. Surface description (table 3-1).....	Grass		
2. Manning's roughness coefficient, n (table 3-1).....	0.24		
3. Flow Length, L (total L ≤ 300 ft).....ft	200		
4. Two-Year 24-hour rainfall, p ₂ in	3.57		
5. Land Slope, s.....ft/ft	0.0250		
6. $T_t = \frac{0.007 (nL)^{0.8}}{p_2^{0.5} s^{0.4}}$ Compute T _t hr	0.36	+	=
			0.36

Shallow Concentrated Flow

Segment ID	B-C		
7. Surface description (paved or unpaved).....	Unpaved		
8. Flow length, Lft	1108		
9. Watercourse slope, sft/ft	0.0397		
10. Average velocity, V (figure 3-1).....ft/s	3.21		
11. $T_t = \frac{L}{3600V}$ Compute T _t hr	0.10	+	=
			0.10

Channel Flow

Segment ID	CD	DE	
12. Cross sectional flow area, a.....ft ²	9.39	15.71	
13. Wetted perimeter, Pw.....ft	11.24	12.4	
14. Hydraulic Radius, r = a/Pw Compute r.....ft	0.84	1.27	
15. Channel Slope, s.....ft/ft	0.0277	0.0182	
16. Manning's Roughness coefficient, n.....	0.03	0.03	
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$ Compute V.....ft/s	7.36	7.86	
18. Flow Length, L.....ft	440	490	
19. $T_t = \frac{L}{3600V}$ Compute T _t hr	0.02	0.02	=
			0.03
Total T_c			0.49
Use T_c (min.)			29.29

Worksheet 2: Runoff curve number and runoff

Project	Mann's Chapel Road Subdivision	By	MAG	Date	2/8/2018
Location	Outfall #2	Checked	BTN	Date	2/8/2018

Check One: Pre-Developed Developed **Pre-Developed Conditions - Outfall #2**

1. Runoff curve number

Soil name and hydrologic group (appendix A)	Cover description (cover type, treatment, and hydrologic condition; percent impervious; unconnected/connected impervious area ratio)	CN*			Area <input checked="" type="checkbox"/> acres <input type="checkbox"/> mi ² <input type="checkbox"/> %	Product of CN x area
		Table 2-2	Figure 2-3	Figure 2-4		
B	Residential (1 acre average lots)	68			12.57	854.8

* Use only one CN source per line

Totals	12.57	854.76
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CN (weighted) = $\frac{\text{total product} = 854.76}{\text{total area} = 12.57}$

Use CN **68.00**

2. Runoff

	Storm #1	Storm #2	Storm #3
Frequency..... yr	2	10	100
Rainfall, P (24-hour)..... in	3.57	6.13	7.67
Runoff, Q..... in	0.94	2.72	3.96

(Use P and CN with table 2-1, figure 2-1, or equation 2-3 and 2-4)

Worksheet 3: Time of Concentration (T_c) or Travel Time (T_t)

Project Mann's Chapel Road Subdivision	By MAG	Date 2/8/2018
Location Outfall #2	Checked BTN	Date 2/8/2018

Check One: Pre-Developed Developed **Pre-Developed Conditions**

Check One: T_c T_t through subarea

Notes: Space for as many as two segments per flow type can be used for each worksheet.
 Include a map, schematic, or description of flow segments

Sheet Flow (Applicable to T_c only)

	Segment ID	A-B		
1. Surface description (table 3-1).....		Grass		
2. Manning's roughness coefficient, n (table 3-1).....		0.24		
3. Flow Length, L (total L <= 300 ft).....ft		200		
4. Two-Year 24-hour rainfall, p_2 in		3.57		
5. Land Slope, sft/ft		0.0700		
6. $T_t = \frac{0.007 (nL)^{0.8}}{p_2^{0.5} s^{0.4}}$ Compute T_t hr		0.24	+	=
				0.24

Shallow Concentrated Flow

	Segment ID	B-C		
7. Surface description (paved or unpaved).....		Unpaved		
8. Flow length, Lft		1141		
9. Watercourse slope, sft/ft		0.0473		
10. Average velocity, V (figure 3-1).....ft/s		3.51		
11. $T_t = \frac{L}{3600V}$ Compute T_t hr		0.09	+	=
				0.09

Channel Flow

	Segment ID	CD		DE
12. Cross sectional flow area, aft ²				
13. Wetted perimeter, P_wft				
14. Hydraulic Radius, $r = a/P_w$ Compute rft				
15. Channel Slope, sft/ft				
16. Manning's Roughness coefficient, n				
17. $V = \frac{1.49 r^{2/3} s^{1/2}}{n}$ Compute Vft/s				
18. Flow Length, L.....ft				
19. $T_t = \frac{L}{3600V}$ Compute T_t hr			+	=
				0.00
				Total Tc 0.33
				Use Tc (min.) 19.67

Appendix B

Treatment Swale Computations

Worksheet for Treatment Swale Section

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.030	
Channel Slope	0.07000	ft/ft
Left Side Slope	3.00	ft/ft (H:V)
Right Side Slope	3.00	ft/ft (H:V)
Bottom Width	1.00	ft
Discharge	2.54	ft ³ /s

Results

Normal Depth	0.30	ft
Flow Area	0.57	ft ²
Wetted Perimeter	2.90	ft
Hydraulic Radius	0.20	ft
Top Width	2.80	ft
Critical Depth	0.40	ft
Critical Slope	0.02163	ft/ft
Velocity	4.44	ft/s
Velocity Head	0.31	ft
Specific Energy	0.61	ft
Froude Number	1.73	
Flow Type	Supercritical	

GVF Input Data

Downstream Depth	0.00	ft
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	ft
Profile Description		
Profile Headloss	0.00	ft
Downstream Velocity	Infinity	ft/s
Upstream Velocity	Infinity	ft/s
Normal Depth	0.30	ft
Critical Depth	0.40	ft
Channel Slope	0.07000	ft/ft

Worksheet for Treatment Swale Section

GVF Output Data

Critical Slope 0.02163 ft/ft

Appendix C

Bioretention Basin Preliminary Sizing

Maximum Allowable Depth		$d_{max} = \frac{f * T_s}{n}$
f (Infiltration rate based on underlying soil) (ft/hr)	0.0166	
Ts (Maximum allowable Storage Time) (hr)	48	
n (Porosity of Soil Media)	0.25	
d _{max} (Maximum Allowable Depth) (ft)	3.1872	

Target Treatment Volume Required		T_v
P	1	
RvI	0.95	
%I	0.3195652	
RvT	0.2	
%T	0.4630435	
RvF	0.03	
%F	0.2173913	
SA (acres)	4.6	
Site Rv (Volumetric Runoff Coefficient)	0.40	
Tv (Target Treatment Volume) (ac.-ft.)	0.154375	
Tv (Target Treatment Volume) (ft ³)	6,725	

Bioretention Area A	
STEP 1 Surface Ponding	
Surface Ponding Depth d _{ponding} (ft.)	1.00
Surface Ponding Volume (ft ³) Must be ≥50% of Design Tv	3978.00
Average Ponding Surface Area (ft ²) (SA _{avg-ponding})	3978.00
Side Slopes (3:1)	3.00
Approximate surface area at the top of the ponding depth (ft ²)	4500.00
Approximate surface area at the bottom of the ponding depth (ft ²)	3456.00

STEP 2 Soil Media Surface Area and Depth	
Soil Media Surface Area (SA _{bottom}) (ft ²)	3456.00
d _{media} (ft)	2.00
d _{gravel} (ft)	1.00
n _{media}	0.25
n _{gravel}	0.4
SA _{avg-ponding} (ft ²)	3,978.00
d _{ponding} (ft)	1.0
DV _{practive} (ft ³)	7,088

Appendix D

Stream Crossing Culvert Computations

Culvert Design Report

Culvert Drainage Area - Discharge Rates

Peak Discharge Method: SCS Peak Discharge

Design Rainfall Depth	6.13 in	Check Rainfall Depth	7.67 in
Design Peak Discharge	91.36 cfs	Check Peak Discharge	125.18 cfs
Total Area	28.26 acres	Time of Concentration	28.31 min
Weighted Curve Number	79	Rainfall Type	Type II

Subwatershed	Area (acres)	CN
1	28.26	79

Grades Model: Inverts

Invert Upstream	528.00 ft	Invert Downstream	526.00 ft
Length	100.00 ft	Slope	0.020000 ft/ft
Drop	2.00 ft		

Headwater Model: Allowable HW/Height

Headwater Depth/Height	0.00
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Tailwater Conditions: Constant Tailwater

Tailwater Elevation	N/A ft
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Culvert Calculator Report

Culvert 1 - 100 yr for Culvert Size

Solve For: Section Size

Culvert Summary			
Allowable HW Elevation	538.00 ft	Headwater Depth/Height	2.34
Computed Headwater Elevation	535.03 ft	Discharge	125.18 cfs
Inlet Control HW Elev.	535.03 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	533.87 ft	Control Type	Inlet Control

Grades			
Upstream Invert	528.00 ft	Downstream Invert	526.00 ft
Length	100.00 ft	Constructed Slope	0.020000 ft/ft

Hydraulic Profile			
Profile	S2	Depth, Downstream	2.14 ft
Slope Type	Steep	Normal Depth	1.95 ft
Flow Regime	Supercritical	Critical Depth	3.00 ft
Velocity Downstream	14.60 ft/s	Critical Slope	0.010230 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	4.00 ft
Section Size	4 x 3 ft	Rise	3.00 ft
Number Sections	1		

Outlet Control Properties			
Outlet Control HW Elev.	533.87 ft	Upstream Velocity Head	1.69 ft
Ke	0.70	Entrance Loss	1.18 ft

Inlet Control Properties			
Inlet Control HW Elev.	535.03 ft	Flow Control	N/A
Inlet Type	0° wingwall flares	Area Full	12.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

Culvert Calculator Report

Culvert 1 - 25 yr for Headwater

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	538.00 ft	Headwater Depth/Height	1.42
Computed Headwater Elevation	532.25 ft	Discharge	91.36 cfs
Inlet Control HW Elev.	532.25 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	532.05 ft	Control Type	Inlet Control
Grades			
Upstream Invert	528.00 ft	Downstream Invert	526.00 ft
Length	100.00 ft	Constructed Slope	0.020000 ft/ft
Hydraulic Profile			
Profile	S2	Depth, Downstream	1.68 ft
Slope Type	Steep	Normal Depth	1.55 ft
Flow Regime	Supercritical	Critical Depth	2.53 ft
Velocity Downstream	13.61 ft/s	Critical Slope	0.005377 ft/ft
Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	4.00 ft
Section Size	4 x 3 ft	Rise	3.00 ft
Number Sections	1		
Outlet Control Properties			
Outlet Control HW Elev.	532.05 ft	Upstream Velocity Head	1.27 ft
Ke	0.20	Entrance Loss	0.25 ft
Inlet Control Properties			
Inlet Control HW Elev.	532.25 ft	Flow Control	Submerged
Inlet Type	90° headwall w 45° bevels	Area Full	12.0 ft²
K	0.49500	HDS 5 Chart	10
M	0.66700	HDS 5 Scale	2
C	0.03140	Equation Form	2
Y	0.82000		

DA = 3.75 Ac
CN = 77
TO Ex. 15" RCP

DA = 3.89 Ac
CN = 77
TO Ex. 18" RCP

S.R. 1532 (Mann's Chapel Rd.)
(60' Public R/W) (Plat 25-54)

DA = 20.22 Ac
CN = 72
TO Ex. POND

DA = 50.70 Ac
CN = 76
TO OUTFALL 1

DA = 12.57 Ac
CN = 68
TO OUTFALL 2

SHELTON G. LLOYD
TAX PARCEL #69889
DEED BK. 1448, PG. V27
PLAT BK. 2007, PG. 176

JAMES C. LINTON COPPER & ROSA SCARBOROUGH
TAX PARCEL #68689
DEED BK. 1921, PG. 240
PLAT BK. 92, PG. 214

JAMES M. JANUARY
TAX PARCEL #63449
DEED BK. 1344, PG. 185
PLAT BK. 34, PG. 23

THOMAS N. HELLMAN II
TAX PARCEL #65588
DEED BK. 1654, PG. 287
PLAT BK. 29, PG. 29

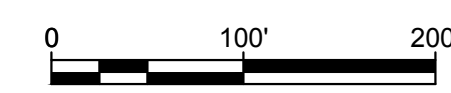
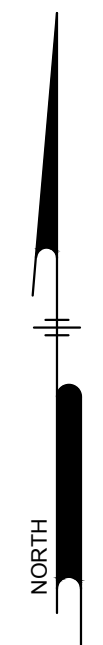
NELSON R. WALL
TAX PARCEL #65570
DEED BK. 1348, PG. 319
PLAT BK. 26, PG. 27

BILLIE W. MEDLIN
TAX PARCEL #62253
WILL 13E-119
PLAT SLIDE A PG. 731

DONALD F. MEDLIN
TAX PARCEL #62259
DEED BK. 1743, PG. 398
PLAT SLIDE A PG. 731

DAVID S. LEEPER
TAX PARCEL #28223
DEED BK. 1497, PG. 57

MNP BRYAR CHAPEL LLC
TAX PARCEL #67089
DEED BK. 1074, PG. 75
PLAT BK. 2009, PG. 218



**PRELIMINARY
NOT FOR CONSTRUCTION**

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ALL DIMENSIONS MUST BE VERIFIED BY CONTRACTOR AND OWNER MUST BE NOTIFIED OF ANY DISCREPANCIES BEFORE PROCEEDING WITH WORK

BONTERRA SUBDIVISION
3954 MANN'S CHAPEL ROAD
CHAPEL HILL, NC 27516

PRE-DEVELOPED DRAINAGE PLAN

IDEAL CAPITAL GROUP, LLC
2100 COOK RIDGE COURT
RALEIGH, NC 27615

NO.	DATE	REVISIONS	BY

PROJECT **DLAZ1701**

DATE **2018-02-16**

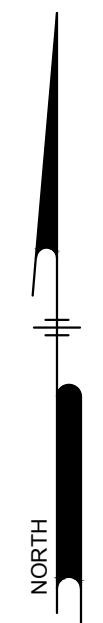
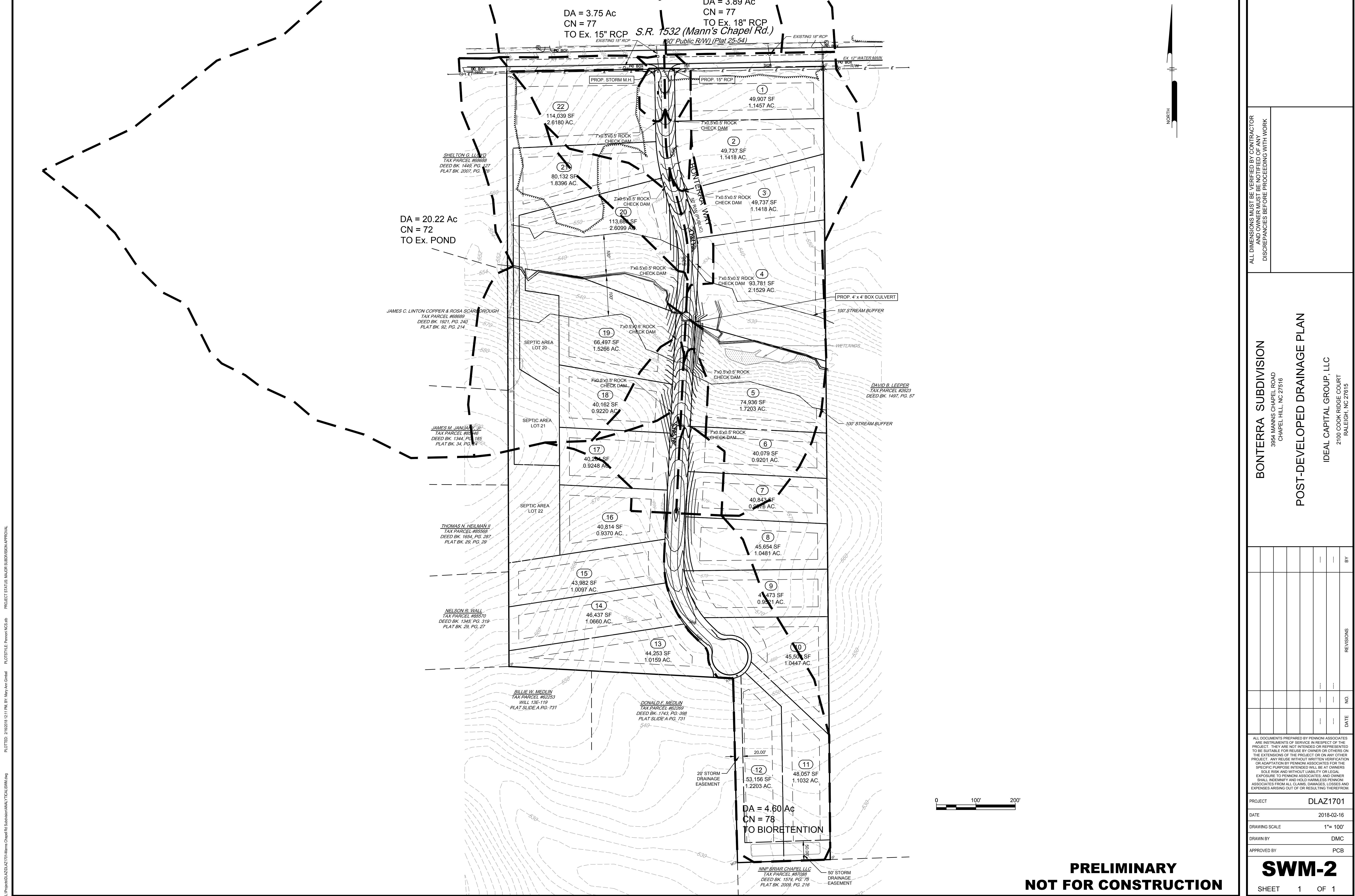
DRAWING SCALE **1"= 100'**

DRAWN BY **DMC**

APPROVED BY **PCB**

SWM-1

SHEET **1** OF **1**



PRELIMINARY
NOT FOR CONSTRUCTION

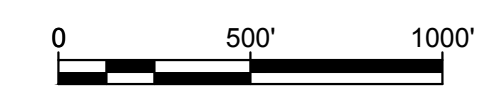
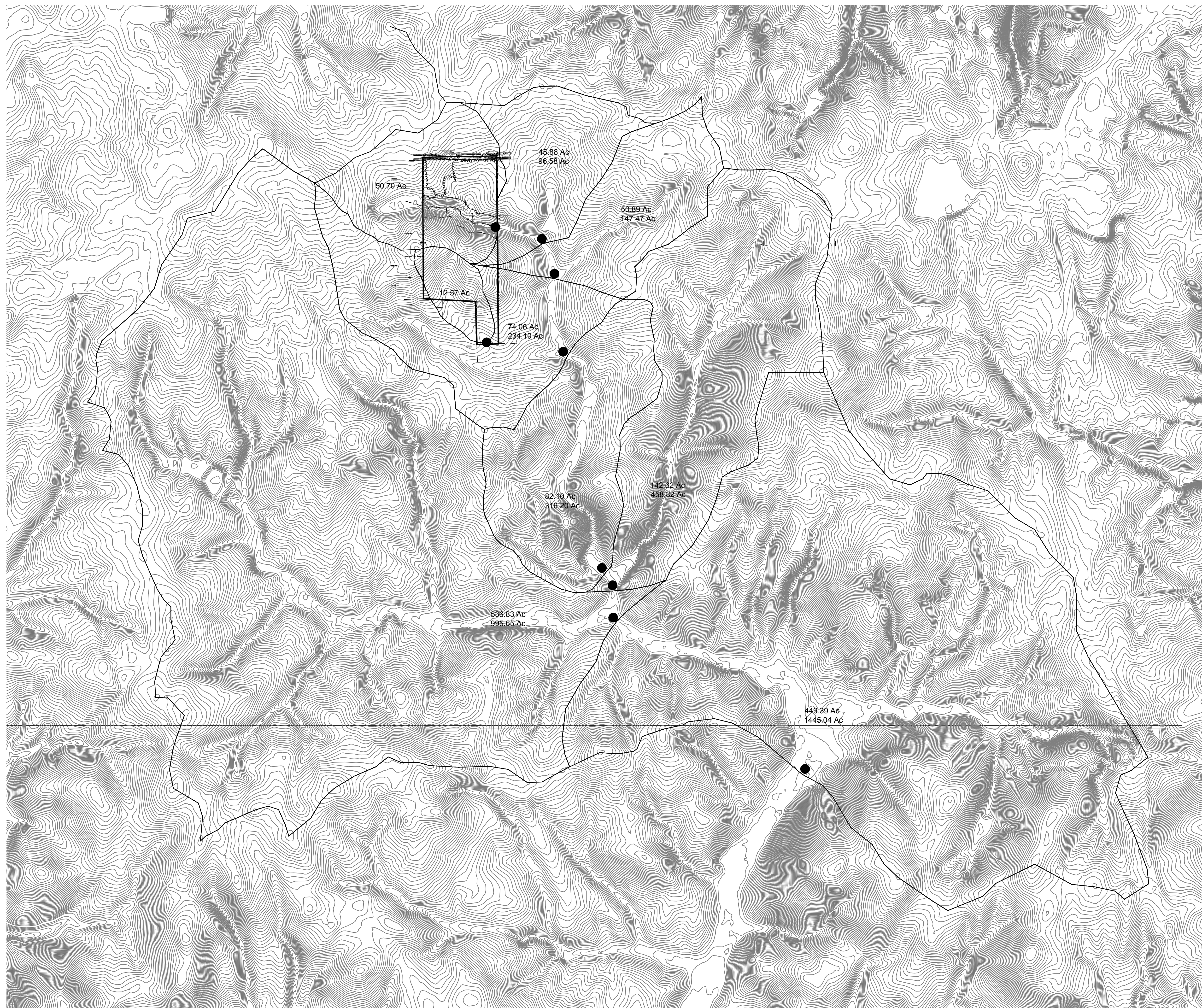
ALL DIMENSIONS MUST BE VERIFIED BY CONTRACTOR
 AND OWNER MUST BE NOTIFIED OF ANY
 DISCREPANCIES BEFORE PROCEEDING WITH WORK

BONTERRA SUBDIVISION
 3954 MANN'S CHAPEL ROAD
 CHAPEL HILL, NC 27516
POST-DEVELOPED DRAINAGE PLAN
 IDEAL CAPITAL GROUP, LLC
 2100 COOK RIDGE COURT
 RALEIGH, NC 27615

NO.	DATE	REVISIONS	BY

PROJECT	DLAZ1701
DATE	2018-02-16
DRAWING SCALE	1" = 100'
DRAWN BY	DMC
APPROVED BY	PCB

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**PRELIMINARY
NOT FOR CONSTRUCTION**

ALL DIMENSIONS MUST BE VERIFIED BY CONTRACTOR AND OWNER MUST BE NOTIFIED OF ANY DISCREPANCIES BEFORE PROCEEDING WITH WORK

BONTERRA SUBDIVISION
3954 MANN'S CHAPEL ROAD
CHAPEL HILL, NC 27516

DOWNSTREAM DRAINAGE DIVIDES

IDEAL CAPITAL GROUP, LLC
2100 COOK RIDGE COURT
RALEIGH, NC 27615

NO.	DATE	NO.	BY

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DRAWN BY	DMC
APPROVED BY	PCB

SWM-3
SHEET 1 OF 1